CARD SHARK

Michigan Technological University

Project Proposal

2023



Michigan Technological University Concrete Canoe Team Grover C. Dillman Hall 1700 Townsend Drive Houghton, Michigan 49931

February 17, 2023

Committee on Concrete Canoe Competitions 1801 Alexander Bell Drive Reston, Virginia 20191 Attn: Technical Proposal Cover Letter

Dear Committee on Concrete Canoe Competitions,

The 2022-2023 Michigan Technological University Concrete Canoe Team hereby certifies:

The hull design, mix design, reinforcement scheme, and construction of the prototype are completed and in full compliance with the specifications stated in the *2023 Request for Proposals*. Our team also has reviewed all Material Technical Data Sheets (MTDS) and Safety Data Sheets (SDS) that the team deems relevant towards this year's prototype. The team also acknowledges receipt of the *Request for Information* (RFI) Summary and that all submissions comply with their provided responses. The anticipated competition participants are qualified student members and Society Student Members of ASCE and meet all eligibility requirements.

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Sincerely,

Jyeha Loney

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For a)

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CARD SHARK 🛃 👷

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Executive Summary

Risk and reward has always been an alluring subject. This is exactly why so many people find themselves in casinos. When enjoyed responsibly, these places bring us together over the joy of spending time with friends. A little bit of risk combined with a lot of calculations goes a long way. This is the metaphor that the Michigan Technological University (Michigan Tech) Concrete Canoe team applied to their boat, *Card Shark*, this year. Statistically, 11% of people make money from casinos (Berzon & Maremont, 2013). This is why the team knew they had to heavily rely on research and development to have a successful boat this year.

The name, *Card Shark*, has been known to imply a meaning surrounded by notions of cheating. This is the exact opposite of the intended meaning. More commonly, when a person thinks of the phrase "card shark" an image of cunning and diligent calculations comes to mind. In addition to all of this, the team believes the name combined a water theme and a larger theme of casino nights with friends.

Michigan Tech's concrete canoe team is not only backed by a strong civil engineering department, but an overall strong engineering department in general. The civil, geospatial, and environmental departments make up 14% of the College of Engineering by enrollment (Michigan Technological University, 2022). This department has always strongly supported the concrete canoe team. In fact, the team's best boat, *Yooper*, is permanently on display in the DOW Environmental building.

In addition, this department has been on the forefront of many Civil engineering projects within nearby Houghton and the greater US. In June 2022, two students of the department worked to get the Portage lift bridge named a national historical site (Weingarten, 2022). The depth that this Civil & Environmental engineering department has is greatly extended throughout its student organizations. The Michigan Tech Concrete Canoe Team is no exception.



Figure 1: Portage Lake Lift Bridge was honored by ASCE as a national landmark in June 2022.

Card Shark is Michigan Tech's most innovative boat in recent years. This has been achieved through careful and calculated changes. 2022's boat, *Kraken*, albeit a practical and simple boat, lacked a keel. The team felt this negatively impacted *Kraken's* ability to paddle straight. In 2022, it placed first in one race, the women's slalom race. This makes sense as this race is an excellent test of maneuverability. The keel on *Card Shark* has been specifically designed to optimize maneuverability and straight-line tracking.

Card Shark	
Colors	Green, Red, and Black
Length	20 feet
Width	2.8 feet
Thickness	0.375 inches
Weight	300 lbs
Primary Reinforcement	SpiderLath
Secondary	GlasGrid 8511 & 1/16 th
Reinforcement	in PT cables

Table 1: Properties of Card Shark

The reinforcement scheme of *Card Shark* has been reimagined. In the run-up to casting day, the team thoroughly tested a brand-new post-tensioning system. This is a new concept for the Michigan Tech team. In past years, a pretensioned cable has been placed in the gunnels. *Kraken* lacked any kind of





cable system. This new cable system was designed to add the needed structural support to the canoe without damaging the prototype. Cables were tensioned to the needed value to allow for maximum support.

A committee was created to model the cables through structural analysis. This needed to be done so the team could find the best placement for the cables within the concrete. Not to mention, the number of cables had to be decided upon. This committee worked closely with the mixture crew to figure out how much force could be placed upon the mixture by the cables.

The mixture committee focused on three qualities with this year's structural mixes. They prioritized strength, weight, and environmentally conscious factors throughout *Card Shark's* mixture design. *Card Shark's* aesthetics were also at the forefront of this year's design. The team designed an exterior that reflected the theme of casino night with card suit inlays along the hull of the boat. These inlays required three different testing cycles to refine the color, workability, and location of the inlays. For the interior of the boat, a semi-transparent green concrete stain was used, alluring to a poker table.

At the top of the team's management scheme is one project manager, in charge of overall construction and process flow, and one deliverables lead, in charge of the display, paper, and presentation. This split in management allows for flexibility between the two positions. The split also ensures one person is not under too much strain.

During the construction of *Kraken*, the team operated under a senior and junior captain. Members found these roles to be too vague. The new management scheme was designed for better efficiency and control over different aspects of competition. Besides the two lead positions, there are a handful of sub-committee heads working on construction, display, or presentation, for example.

Sustainability remains at the forefront of Michigan Tech's construction processes. When designing *Card Shark*, the team utilized melted snow as their source of water. The team also relied on recycled concrete for many of its test mixes.

The Michigan Tech concrete canoe team is eager and pleased to present their 2023, *Card Shark*, as an example of how far a little bit of risk and a lot of calculation can take a design team.

Mixture	Unit W	Unit Weight (pcf)		h (psi)					
	Wat	Oven-	Compressive		Tensile		Air Content (%)	Slump	
	Wet	Dry	14-day	28-day	14-day	28-day	(70)	(in.)	
Primary Structural	70.2	64.7	1470	1600	250	290	0.1	1.0	
Secondary Structural	72.1	66.2	1380	1520	210	240	0.1	1.0	
Pigmented Finishing	74.9	69.9	930	1000	200	220	0.1	1.5	
28-day Composite Flexural Strength: 1040 psi									





Chapter Profile

Michigan Technological University is a public, mid-level research university located in the town of Houghton, near the top of the Upper Peninsula of Michigan. Founded in 1885, the university offers a prestigious STEM education for its over seven thousand students (Michigan Technological University, 2022).

Michigan Tech's student ASCE chapter currently has 146 student members, with 83 being registered national members. Once every month, the school's ACSE chapter hosts a meeting in which school faculty and industry partners are invited to speak about their engineering experiences while exposing the student members to the field. ACSE aims to increase its student engagement even more by hosting these meetings.

Alongside said meetings, the chapter and University organizes "Make a Difference Day" on campus, where student organizations gather to make a positive impact on the local environment and community. A few other projects that ASCE has participated in include the Adopt a Highway program, where students are assigned to clean up a two mile stretch of road, as well as cleaning parks, raking leaves in the community and working at local food pantries.

Since 1992, the Michigan Tech Concrete Canoe team has competed in the North Central Student Conference, placing first in 10 out of the last 11 competitions. In 2022, the team competed in the Eastern Great Lakes Conference and placed 3rd overall in the regional competition.

In addition, Michigan Tech's Steel Bridge Team competes in the annual ASCE Steel Bridge Competition. The Michigan Tech Steel Bridge Team earned 2nd place overall at the 2022 North Central Regional Competition, allowing them to continue to the national competition. The team placed 1st in Economy, 2nd in Construction Speed. 3rd on Efficiency and Stiffness and 4th in Lightness. At the national competition, the team placed 5th.

Figure 2: The Michigan Tech Concrete Canoe Team at the 2022 Regional Symposium





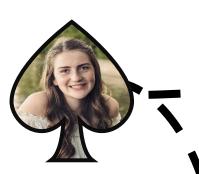
Key Team Roles

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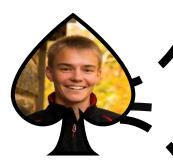
Michigan Tech's concrete canoe team underwent a redesign of its team structure. During the construction of the team's 2022 boat, *Kraken*, the team was led by a sole project manager. At the conclusion of the 2021-2022 school year, the team met to discuss a different management scheme. This discussion resulted in the following team structure:

Key Member and Role	Responsibilities
Project Manager: Lydia Lamey	Meetings
	Scheduling Technical Proposal
	Scheduling
Deliverables Lead: Samuel Pendell	Technical Presentation
	Fundraising
Treasurer: Patrick Mungcal	Outreach
	Budget
Paddling Coordinator: Colin Vanderbeek	Paddling Practices Prototype Demonstration
T dualing Coordinator. Com Vanderoeek	Technical Presentation
	Lab Cleanliness
	Final Mixture Design
Lab Supervisor: Connor Dykehouse	Technical Proposal
	Curing Process
	PPE Manager
	Mix Research and Development
Mix Design Lead: Duffy Karstrom	Final and Finishing Mixture Design
Mix Design Leua. Durry Karsuoni	Sieve Analysis
	MTDS
Structural Analysis Lead: Jacob Byron	Structural Analysis
Sir uctur ut Analysis Leau. Jacob Byton	Tensioning System Design
	Prototype Dimensions
Hull Design Lead: Max Hazen	Displacement and Drag Calculations
man Design Deau. max mazen	Technical Proposal
	Mold Preparation
	Three-point Bend Tests
Reinforcement Design Lead: Jake Hazel	Reinforcement Scheme
	Structural Analysis
Aesthetics Leads: Suraiya Siddiqi and Alicja	Stands & Display Construction
Grzegorzek	Prototype Finishing
	Compliance
QC/QA Lead: Luke Sturm	Quality Checks
	Sieve Analysis
Safety Lead: Sydney Laforest	Lab Training & Tours
	PPE Manager





Lydia Lamey, So. Project Manager & Captain Oversaw all constructionrelated committees. Worked with: Max Hazen, Jr., Jacob Byron, Sr., Jake Hazel, So., and Duffy Karstrom, Jr.



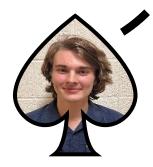
Connor Dykehouse, Sr. *Lab Supervisor* Oversaw all lab activities and developed final mix. *Advisor:* Dr. Tess Ahlborn Assisted with any questions. *Presenters:* Sydney Streveler, Jr. Samuel Pendell, So. Luke Sturm, Jr. Lauren Kubow, Fr.



Duffy Karstrom, Jr. Mixture Design Lead Oversaw design of structural and finishing mixes



Samuel Pendell, So. Deliverables Lead & Captain Oversaw all academic related committees. Worked with: Lydia Lamey(paper), So., and Colin Vanderbeek(presentation), Sr.



Colin Vanderbeek, Sr. *Paddling Coordinator* Oversaw paddling practice and conditioning.



Luke Sturm, Jr. QC/QA Lead Oversaw all compliance checks and ensured project met RFP requirements.



Suraiya Siddiqi, Jr. Aesthetics Lead Oversaw all finishing elements of prototype, stands, and display design. Assisted by: Alicja Grzegorzek, So.



Sydney Laforest, Sr. Safety Lead Ensured all processes followed proper safety guidelines.



Technical Approach

Hull Design

This year, the hull design committee focused on achieving two goals: developing a prototype that met the RFP requirements and improving upon last year's canoe, *Kraken*. This first goal was met with a thorough reading of the RFP requirements. A length of 20 feet was decided upon because it would allow for enough displacement while also falling within the guidelines.

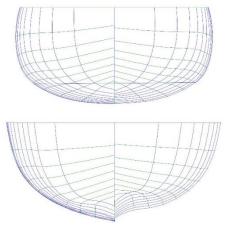
Last year, a more conservative and traditional design approach was used when creating Kraken. Kraken featured a flat bottom with moderate curves, allowing for a more forgiving ride to paddlers. This also resulted in increased maneuverability during the slalom races, as reported by the paddlers. High total displacement of approximately 1930 lbs. and a higher overall block coefficient of 0.431 allowed for greater stability. Despite having a higher optimum speed than Card Shark, the paddlers had to use more energy to steer the boat, preventing Kraken from reaching a higher speed. This effect was worsened by drawbacks that occurred during last year's construction process. The team had to improvise the reconstruction of each endcap of Kraken due to difficulties that arose during the de-molding process. Because of this, Kraken suffered even more in straight-line tracking.

A combination of qualitative experiences and simulation durations from 2022's prototype demonstrations allowed the hull design committee to come to a consensus. To improve upon last year's prototype, a design with higher displacement and straight-line tracking was developed.

Using a canoe template provided in the CAD software, Prolines8 ®, we began to contour the boat. *Card Shark* features two shallow channels running down the bottom of the hull, with a short keel in the middle. The keel doesn't run the entire length of the canoe as the paddlers felt this would lead to difficulty turning. As *Card Shark* traverses, water is directed through the channels that coincide with the direction

of travel. The keel also coincides with the direction of travel. Both features increase resistance to any motion from paddlers that is not in the direction of travel. The intention of this design was to promote better straight-line tracking. Paddlers would be able to spend more energy towards speed rather than steering the canoe.

Figure 3: Hull Comparison, Kraken above and Card Shark below, to scale, left of diagrams: bow view, right of diagrams: stern view.



Because of these features, *Card Shark's* walls are wider, and this resulted in a deck beam of 2.823 ft. The keel and channels also resulted in a higher surface area of 64.840 ft². Using a safety factor of 1.25 and by assuming the boat would have a weight of 300 lbs., a conservative ballast of 375 lbs was calculated. This led to a combined weight of 675 lbs. Using Prolines8®, the following properties were calculated:

Table 3: Hull	Design	Comparison
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Property	Kraken (2022)	Card Shark (2023)
Length (ft)	20.0	20.0
Max Deck Beam (ft)	2.41	2.82
Max Freeboard (ft)	0.684	0.640
Male Race Displacement (lbs)	580	675
Block Coefficient	0.410	0.334
Optimum Speed (knots)	4.46	4.01





In comparison to 2022's boat, *Kraken, Card Shark's* design is better suited for sprint-style races. However, it does not completely sacrifice the ability to make hairpin turns as required in the Prototype Demonstration.

Structural Analysis

After *Card Shark's* hull design was decided upon, the structural analysis committee set out to provide the material development committee with some baseline information. This included necessary material requirements and the future location of the six steel cables. The minimum compression value of the concrete cylinders also needed to be found.

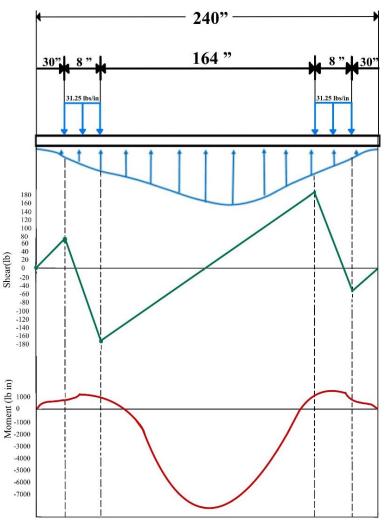
The men's sprint was used in the analysis as a baseline for the punching shear and flexural stress under load. Using our hull design software Prolines 8®, we found the resultant force of 811.39 lbs. over an area of 42.014 ft^2 . When conducting the 2D structural analysis of our hull design under load, the following assumptions had to be made:

- 1. Paddlers in the stern and bow sit an equal distance from both ends.
- 2. The uniform thickness of the canoe is 0.375 in or 3/8 inches throughout.
- 3. The paddlers both sit on the centerline of the canoe allowing us to neglect torsional stresses.
- 4. The assumption is that both paddlers weigh 250 lbs. each and are distributed over an 8" by 12" area for a seat position.
- 5. The area for the moment of inertia was calculated as a C-channel, neglecting the Gunwale of the canoe.
- 6. The canoe's weight was approximated using the number of mixes and the weighing of individual components such as the mesh/foam/cables/and plates.
- 7. This was also assuming that the canoe is static under the load of the weight of the paddles, canoe, and bouncy force of the canoe.

Hand calculations were completed for the shear and moment diagrams. The shear stress was

calculated by applying the loads in a 2-D analysis. The shear diagram was then used to determine the moment diagram. The punching shear was then calculated at the critical location of 202 inches from the bow of the canoe. Resulting from these calculations was a value of 491,902 psi for maximum flexural stress at a location of 117.3 inches from the bow. The punching shear was calculated by modeling an area of 8" by 12" under a sitting load. Men's weights were conservatively given a value of 250lbs. A punching shear stress of 12 psi at a location of 202 inches from the bow was determined using the shear diagram. It was found through ACI 318 Table 19.2.4.2 and Table 22.6.5.2 that our concrete's capacity was 241.11 psi, showing our punching shear load of 12 psi is well within our concrete's capacity (ACI).

Figure 4: Structural Analysis







From these findings, the team recognized they needed to account for flexural stress. This was accomplished with the usage of two types of reinforcement mesh, along with a tensioning system.

The team found a reinforcement scheme that had an average flexural strength of 240 psi. The remaining strength needed (to counteract the calculated 491 psi flexural stress) came from the tensioning system.

Six 1/16" cables were uniformly distributed throughout the hull of the canoe. These cables were placed between the two types of mesh. Specifically, one set of the cables was placed near the gunwales to account for flexural stresses. Michigan Tech's 2019 boat, *Driftwood*, experienced cracks in the middle due to torsional stress while turning (MTUCC, 2019). This is what led the team to use a cable in the gunwales in 2020's boat, *Dozer* (MTUCC, 2020). This cable was pre-tensioned, meaning it would only prevent cracks from worsening. The other two sets of cables in the prototype were also post-tensioned to the same force of 80 lbf.

Mix design and Testing Protocol

The primary goals of the mixture committee this year included developing a final mix that is less dense than water, acquiring, and incorporating new materials into our mix designs. The committee also made it a priority to create a final mix that meets the gradation requirements from the sieve analysis while also having good workability for our trowelers. The team worked towards these goals in a step-by-step process that began with an in-depth review of this year's RFP.

Shortly after this year's competition rules were released, the mixture committee identified the sieve analysis gradation requirements as an addition to the competition rules and a requirement that could potentially cause some difficulty. In previous years, our team had used large amounts of very fine aggregate materials that are low in density such as K1 and K37. These materials were also shown to be beneficial to the trowelers because they are very finegrained and much easier to trowel than other coarsergrained aggregates. The mix committee identified that these materials were no longer considered mineral filler and that the amount of K1 and K37 that was used in previous years mixtures would have to be significantly reduced to ensure less than ten percent of the composite aggregate material did not pass the number 100 sieve. New materials were immediately ordered to account for this.

The mixture committee developed and researched a list of new materials to consider incorporating into our mix designs. Three different gradations of Hess Pumice (ASTM C330) were ordered: Pumice #3, Pumice #5, and Pumice #7. This type of aggregate material was selected due to its low density and tested in various mix designs throughout the fall semester. In addition to aggregates, the mix committee ordered Metakaolin (ASTM C618) to be used as a supplementary cementitious material in our mix designs. Metakaolin is shown to have high early age strength as well as having the lowest density of all our binder materials (Justice & Kurtis, 2007).

Due to the inexperience of our mix committee, recruiting new members was emphasized early in the year. Mix committee leads held information sessions detailing how mixture designs were created and adjusted. After completing the required training, new members of the team were taken to our lab and shown how to measure out, mix, and then properly fill concrete test cylinders (ASTM C192). Team members were also shown how to operate the concrete compression machine. The emphasis the mix committee placed on knowledge transfer helps set up the team for success in future years.

Sustainable practices were thoroughly incorporated into the mix committee's operations. In previous years, the team would make 8-cylinder concrete batches when testing different designs. This year, 4-cylinder batches were used to help reduce waste while still providing an adequate quantity of cylinders to test at 7- and 14-day intervals. Cylinder molds were also reused with the help of a release agent and a small hole in the bottom of the molds, allowing for an air compressor to gently remove the concrete cylinder. Lastly, recycled crushed concrete was used from previously tested mixes as an aggregate in the committee's mix designs. Using this





recycled material helped reduce waste as well as incorporate a material that is produced frequently throughout the fall semester.

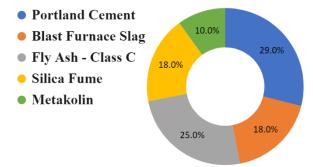
Throughout the testing process, concrete cylinders were filled (ASTM C192) for every individual concrete mixture and the cylinders were submerged in water for the first seven days. This promoted better hydration of tricalcium silicate, which is associated with concrete's initial setting and early strength development (Garrault at al., 2005). The cylinders were then tested at seven- and fourteen-day intervals for compressive strength (ASTM C39) and unit weight (ASTM C138). Predominant attributes from *Kraken* (MTU Concrete Canoe Team, 2022) were used to establish a baseline for this year's structural mix testing. After obtaining the unit weight and compressive strength of our baseline mix, testing began using a tiered system.

In the first tier of testing, the binder ratios were adjusted slightly with each mix while the remaining components of the mix were held constant. The results of our binder tier testing are shown in table 4. The tests highlighted in red were immediately disregarded, regardless of their unit weight, because they were considered too difficult to trowel. Using the data from table 4 as well as qualitative notes about the workability of the different mixtures, mix B7 (table 4) was selected as our final binder blend. Our testing indicated that a hydraulic to pozzolanic ratio of approximately 0.57 vielded the best compressive strength results. A breakdown of the binder mass composition that was used in our final primary structural mix can be found in figure 5. A large percentage of Portland Cement was used due to its high early strength test results, while remaining below the competition maximum of 30% by mass. Large amounts of Class C Fly Ash were used due to its combination of hydraulic and pozzolanic properties. Incorporating Metakaolin and Silica Fume was shown to lower the concrete density as well as serve as a pozzolanic supplementary cementitious material that could react with the other hydraulic materials such as Portland Cement, Blast Furnace Slag, and Class C Fly Ash.

Binder Test Number	Cylinder Mass (grams)	Unit Weight (lb/ft3)	14 Day Comp. Strength (PSI)		
B1	743.9	66.8	1529		
B2	690.3	62.0	952		
B3	708.5	63.6	1111		
B4	718.9	64.6	1453		
B5	728.5	65.4	1273		
B6	748.8	67.3	1550		
B7	681.4	61.2	1375		
B8	704.2	63.3	1490		

Table 4: Binder Tiered Testing Results

Figure 5: Binder Composition by Mass



Aggregates were tested in a similar fashion. The results of our aggregate tier testing is shown in table 5. This data, as well as our notes on the workability of the mixtures, allowed us to determine that mix A12 (table 5) was our best aggregate blend. A breakdown of the aggregate volume composition that was used in our final primary structural mix can be found in figure 6. Most of our aggregate volume was comprised of different gradations of Poraver due to the materials' combination of high strength and low-density test results. The K1 and K37 aggregates, as well as the different gradations of Pumice were incorporated due to low density test results. All our aggregate materials are relatively round, as opposed to angular, which makes placing the concrete much easier on the troweling team.

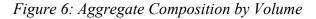


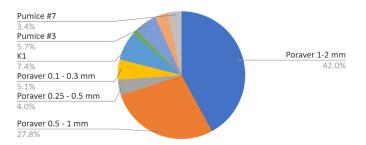


Aggregate Test Number	Cylinder Mass (grams)	Unit Weight (lb/ft3)	14 Day Comp. Strength (PSI)
A1	632.7	56.8	719
A2	722.2	64.9	1113
A3	776.7	69.8	1298
A4	753.2	67.7	1592
A5	741.7	66.6	1439
A6	812.7	73.0	1706
A7	812.3	73.0	1655
A8	775.9	69.7	1619
A9	767.6	68.9	1607
A10	721.0	64.8	1304
A11	784.5	70.5	1521
A12	738.3	66.3	1571
A13	822.2	73.9	1526
A14	730.1	65.6	1490
A15	797.4	71.6	1584

Table 5: Aggregate Tiered Testing Results

The binder and aggregate blend were both utilized to create an optimized final tier of testing. NYCON PVA RFS400 and NYCON PVA RF4000 fibers were used throughout testing and a 60/40 blend was used to lessen the difficulty of troweling. Water to cement ratios of 0.36, 0.38, and 0.40 were tested. A final ratio of 0.38 was selected based on a combination of strength and workability factors. The conclusion of these final tests resulted in this year's primary structural mix, *Two Pair*.





BASF MasterGlenium 7500 was used as a full-range water reducing admixture to improve the workability of the concrete and allow for the water to cement ratio to be reduced, thus increasing the

concrete compressive strength. The full-range water reducer also improves early age strength. BASF MasterSet DELVO was used as a set retarder to give the trowelers more time to place the reinforcement and cables before the concrete set. The manufacturer recommended dosages were used for all admixtures.

In addition to the primary structural mix, the mix committee decided to design and place a secondary structural mix that was used on the third and final inside layer of the canoe. This mix was very similar to the primary structural mix, however, coarser aggregates such as Poraver 0.5-1.0 were reduced or removed to ensure that the trowelers were able to easily create a smooth finish on the inside of the canoe.

Finally, a finishing mix was designed to create a single 8-cylinder batch of concrete that would be used for the inlays on the boat. Large percentages of Blast Furnace Slag and Metakaolin were chosen due to their light color. Finer aggregates were used to allow the concrete to be easily applied. Red and black concrete pigments were added for color.

Reinforcement Design and Testing Protocol

This year, the team decided to spend their time reaffirming last year's reinforcement scheme used in *Kraken*. They also wanted to improve the structural integrity of the prototype with the implementation of a post-tensioning cable system. Finally, the team aimed to better their testing capabilities with a new reinforcement mold.

Two types of mesh, GlasGrid 8511® and SpiderLath were chosen for *Card Shark*. Both methods have been used in past boats to great success. *Kraken (2021)* experienced no major cracking. Previous three-point bend tests showed SpiderLath having the worst seam strength and greatest continuous strength (MTUCC 2020). Keeping this in mind, the reinforcement committee decided to use GlasGrid for its greater seam strength. Three-point bend tests were completed with a SpiderLath/GlasGrid layering scheme. The values found from these tests confirmed the team's decision





to stick with a SpiderLath/GlasGrid (SL/GG) layering scheme. Using a SL/GG scheme, the average flexural stress tests last year yielded a value of 263 psi while this year's yielded a slightly lower value of 241 psi. This could be due to the smaller sample size and different mixture used during the 2022-2023 testing period.

The design of the post-tensioning system began early in the school year. Once a general plan was made, the team met to cast a practice end cap with an anchor point. The first design used ¹/₄" diameter steel cables. The trowlers reported difficulty with achieving lamination between the two reinforcement layers because of the large diameter cable in between. This created delays and led to prematurely setting concrete, preventing the proper bond between layers. The second design used a smaller 1/16th diameter cable. This practice resulted in better bonded layers, but there was still a delay due to the tying of cables between the layers. For placement day, cables were tied to the layer of GlasGrid prior to placement to eliminate any delay.

A new reinforcement mold for three-point bend tests was constructed for more precise tests. The previous mold was warped and led to noncohesive beam sizes. The new mold was constructed with plywood and epoxy to add to its longevity.

Figure 7: 3-Point Bend Test Mold



Construction Process

Michigan Tech's construction process started with multiple practice sessions with the whole team

present. These sessions focused on concrete placement, working with different reinforcement types, mixing the concrete, and group dynamics. These sessions offered invaluable experience to each member, preparing them for the final concrete placement. During these practices, members got to apply their health & safety knowledge that had been outlined in the required lab safety program. Once all new members felt confident in their capabilities and the team felt ready for the final placement, these skill sessions were discontinued so the team could focus on physical preparations for casting day.

The physical preparations began with the decision to choose a high-density foam (HDF) material for the canoe form. Current members remembered casting with foam to build 2022's boat, The Kraken. HDF is an easier material to work with and can be CNC milled to exact specifications. Other materials like wood were considered; however, wood takes considerably more time to work with which makes it inefficient and costly. The HDF came in This made the form four sections more maneuverable as opposed to a wooden basis. This year, the team continued to use a female-style mold. The concave form allowed the team to cast the gunnels and end caps during the initial concrete placement. The concrete used to make the gunnels cured in conjunction with the rest of the boat. The team was also able to achieve a smooth finish along the exterior of the boat, limiting sanding time.

After the mold arrived, the team began prepping the individual sections for construction. This started with an initial application of a thin layer of a spackle-type product to fill in any impurities in the foam. After curing, the layer was sanded and cleared off with pressurized air. The team applied thin layers of epoxy in 24-hour increments with sanding in between. All grits used in the sanding process were predetermined from future years. Sanding began with an aggressive 80 grit paper and gradually moved up to 220 grit. Team members working on mold construction consulted with the mix committee to ensure the mold would not be too slick for concrete to stick during the placement process. The individual pieces were prepped, and a small group of members gathered to assemble the





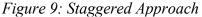
final mold. The pieces were roughly joined before the mold was permanently assembled. Inlay placeholders were positioned into their final locations. A thickness of 1/16th inch was chosen for the inlays. Cardstock was cut out, stacked, and then wrapped in duct tape to prevent any bonding to the concrete.

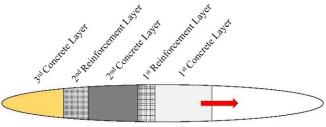




The team used a fine-tuned method for the placement of concrete and reinforcement. The method started with the readying of all materials needed for casting day. Members completed one hour shifts to "pre-batch" all mixtures that would be required on casting day. The reinforcement was precut and measured, along with the cables used in the post-tensioning system. After this was done, the reinforcement materials were pre-formed to the HDF mold, These processes ensured the team could focus on constructing the boat instead of measuring materials and cutting reinforcement during casting day. This eliminated issues like running out of mixture or prematurely setting concrete that could arise during the placement process.

Concrete placement proceeded on a step-bystep basis. The team started off with a 1/16th inch of concrete, followed by a mesh of Glasgrid®8511 reinforcement. This middle layer contained the team's cables and once placed is followed by a 1/8th inch of concrete. The team placed a mesh of Spider lath reinforcement followed by a final 1/8th inch of concrete. This was all accomplished through a staggered approach to reduce cold joints. Trowelers started on one end of the boat and worked towards the other. Once a layer was placed, reinforcement is installed where possible even if the initial layer is not in place over the entire boat. Once all layers were placed, the quality assurance team checked over the final layer, ensuring the smoothest possible finish.





The canoe was cured in a new curing tent in accordance with ASTM C511 standards. The new tent allowed for more humid curing conditions. In the past, the team used a rudimentary set up that involved draping a tarp over the boat. The team believed the previous set-up, although effective, lacked the efficiency that a more air-tight tent could provide. This is why the team built a new structure made of wooden rafters that can be placed over the mold to hold up a tarp. Ultrasonic humidifiers were then placed within this tent. The team achieved a temperature of 75 within the curing tent. The humidity was kept above 95%. This initial curing process continued for 2 weeks.

Mold removal occurred in a delicate manner. The mold pieces were un-screwed and released from each other. Along the gunnels, thin wedges were inserted between the mold and concrete to help release the boat from the mold. This was gradually repeated to deeper depths until the boat was finally free of the mold.

Once free of the mold, the steel cables were tensioned. The team carefully tensioned the cables to 80 lbf of force. After inserting the flotation foam into the end cap, the end cap was sealed off with extra reinforcement to prevent any negative effects that may arise from a cold joint.





The inlays located on the outside layer of the concrete were filled in with the respective finishing mixes before any sanding could occur on the outside of the boat. The inlay locations were inspected for any potential cracks before filling them with pigmented mix.

The aesthetics committee began the process of sanding the interior of the canoe soon after the canoe was inspected for any structural discrepancies. After the prototype passed inspection, any fibers sticking out were clipped. The inside of the boat was initially sanded with a 120-grit sandpaper and slowly progressed up to a 1000 grit sandpaper with water. The outside of the canoe was also brought to a 1000 grit level. The aesthetics committee stained the inside of *Card Shark* with a semi-transparent green color to add more color to the interior of the boat. After a final 10-day cure in normal conditions, a concrete sealer was applied to the entirety of the boat to prepare it for the prototype demonstration (ASTM C309).

Scope, Schedule, and Fee

The Concrete Canoe team is headed by a Project Manager and a Deliverables Lead, each in charge of maintaining specific sections of the committees. The Project Manager (PM), while acting as the main team captain, works closely with the team committees to ensure the project has the correct outcomes. The Deliverables Lead (DL) also works with said committees to ensure that the team sticks to the schedule while also securing the correct information gets submitted. More specifically, the PM oversees construction while the DL focuses on paper and presentation.

The project schedule is developed as early as possible by the PM and DL. The schedule is made using outlines from previous successful years, separating research and development into the fall semester, while the competition display and aesthetics land into the spring semester. This process allows the PM and DL to reflect on the previous year and make changes as they see fit.

After forming a schedule, fundraising for the upcoming year begins. A team newsletter is sent out to known alumni, parents, and donors. The purpose of the newsletter is to update those interested in the upcoming year and to ask for funding. The donations garnered from the newsletter help considerably. The treasurer reaches out to various departments for further donations. The budget is primarily dedicated to buying construction materials and regionals accommodations. This means that material purchases need to be planned out with the project manager and treasurer to ensure there is enough money left in the budget for the regional symposium.

Some of the major milestones occurring during the length of the project include selection of the final structural mixes, finishing mix, and reinforcement scheme, along with the completion of the technical proposal and presentation. Milestones were determined by their importance on the critical path, with the most important moments being decided as a milestone. The team meets these milestones by carefully coordinating the project while having constant communication with the Project Manager. The actions that form the critical path must be completed by their respective deadlines for the project to finish on time. These actions were chosen based on if the project could not continue based on their completion.

Quality Control and Quality Assurance

The construction of a successful prototype is only possible with diligently set protocols ensuring all processes are completed correctly. An engineering team should be able to replicate their projects exactly. This is one goal the Michigan Tech team kept in mind when designing this year's prototype. The team continues to build off previous year's quality control and quality assurance (QC/QA) programs.

For Michigan Tech, this starts when a team member is assigned the role of overseeing QC/QA. This person is charged with a multitude of roles that are fulfilled during concrete mixing, reinforcement testing, construction, and all finishing processes.

During the construction of 2022's boat, *Kraken*, Michigan Tech used melted snow water to save on water usage. This year, to further purify this water, it was strained through a sanitized sheet of a



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high thread count. The sheet was swapped for a clean sheet between batches of water. These processes exemplify the team's desire to control every aspect of the concrete mix.

The concrete mixes were further regulated during the pre-batching process. Each batch was measured out a week before placement day. This allows the team to spend extra time ensuring each material used was a precise weight.

Concrete placement day is the most demanding day for QC/QA. The team recognizes this and creates a schedule of QC/QA tasks to be followed during casting day. Routine layer checks



completed are continuously during the placement of concrete. This is done 3D using printed depth-gauges created by a team member. If the concrete is too thick, a circle will appear on the hull. This process was used during the construction of Kraken: however. the team felt the time intervals could be more

Figure 10: Placement day

structured and stuck to a 5-10 minute schedule. This process ensures the boat will have a uniform thickness.

The QC/QA lead is also charged with compliance review. They work closely with all aspects of the project to ensure that each material used is meeting the required specifications. With this year's requirement of a sieve analysis, the QC/QA lead ensures each aggregate meets the required passing rate.

Knowledge transfer continues to be at the forefront of Michigan Tech's mission. This year, the team met this goal through training sessions. This allowed the QC/QA lead to train in new members with the proper troweling technique and methodology. Focus is on uniform layers and learning to work with different types of reinforcement. This was applied during casting day and helped the team to achieve a uniform thickness of 3/8" throughout the canoe.

Sustainability

The Michigan Tech concrete canoe team is aware of the need for the concrete industry to transition to a more sustainable future. It is estimated that concrete industry contributes 8% of total emissions to the globe (Rodgers 2018). Not to mention, there are various social and economic impacts pertaining to job security and wage-fairness. The team addressed each pillar of sustainability: social, economic, and environmental.

Knowledge transfer is a major goal of Michigan Tech's and directly aligns with social sustainability. Without the pass down of knowledge, the team would have nothing to build off. More innovations can be made if less time is spent on relearning processed. This conserves valuable time and energy.

The pandemic greatly tested the team's ability to transfer knowledge. During the 2022 competition season, there were only a handful of members that had seen real competition on the team. The 2021-2022 school year was spent re-learning and building a wealth of resources that could be used by following teams. This was done through the creation of numerous "how-to" documents, describing the processes of constructing a canoe. By doing this, knowledge is thereby sustainably conserved for the convenient usage of future teams.

Economically, the team transitioned to a more structured inventory scheme. This means the team took a more detailed approach to understanding how much their stockpiles were worth and the lifespan they had left of a certain item. This was accomplished at the beginning of the year with a thorough survey. The inventory was updated periodically throughout the year.





Finally, the team continued with their use of snowmelt as a source of water in the final prototype. This brought up a few initial concerns with the

possibility of the contaminants in mixture; however, this was remedied with the usage of a sustainable filtering system. Overall, the team saved a total of 15 gallons of water. This exercise puts into perspective how much water the concrete industry uses. In the following years, the team the team hopes to expand



Figure 11: Snow melting for placement day

on their sustainable practices, whether they are socially, economically, or environmentally sustainable.

Health & Safety

The Michigan Tech team approaches the health & safety of the team with the utmost sincerity. This begins with naming a person on the team with the role of safety lead. From paddling to construction, this person oversees all processes safety related. At the start of the year, this person oversees lab training. It is their job to make sure each person on the team is up to date on various protocols employed in the team's lab space. Each member must complete a thorough training module and attend a lab tour. This allows members to get acquainted with the lab space before working in it. The safety lead also briefs the members at each weekly meeting with any reminders for the lab. While working in the lab, long pants, close-toed shoes, and safety glasses are a requirement. The Occupational Safety & Health Administration (OSHA) is referred to for all guidelines.

During paddling practices, each paddler is equipped with a life jacket and briefed on what to do if a canoe were to flip. A member of the team is always on shore as well. The team relies on Michigan Tech's water safety protocol for guidelines. Materials testing is another core part of the safety program. Proper personal protection equipment (PPE) is always employed. For concrete mixers, they must always wear gloves, safety glasses, and respirators. During reinforcement tests, members are also required to wear gloves and safety glasses, even if they aren't in the normal lab space.

Before placement day, the team is reminded of proper PPE to ensure everyone arrives with the proper clothing. On the day of, members are once again briefed on safety procedures. These include wearing the proper lab PPE, effective and clear communication, and overall coordination between the different aspects of construction. For example, the reinforcement team needs to remind members not to handle any reinforcement without wearing gloves.

During the sanding and staining of the canoe, extra care is taken. Members are equipped with respirators during any sanding and are not allowed to sand for over an hour at a time. Per the manufacturer guidelines for staining concrete, any person staining the boat is required to wear full PPE including chemical goggles, a respirator, and chemically resistant gloves. The team lab manager also coordinates with faculty for assistance with the application of the stain.

The pandemic greatly impacted the team's ability to function during the 2020-2021 school year. This led to the inability to make a canoe during that year. The effects greatly decreased during the 2021-2022 school year as Michigan Tech transitioned to an in-person learning schedule and classes resumed as normal. Mask restrictions were lifted during the spring semester. This school year, 2022-2023, continues the trend of relaxing restrictions and the team experiences little to no restrictions because of the pandemic.

The health of each member remains a top priority. This is why the team continued to employ the usage of masks when exposed to a possible case of Covid-19. Members were encouraged to alert each other when they tested positive and socially distance when needed.



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Value and Innovation

The Michigan Tech concrete canoe team strives to add value to each product they create. The team also believes value stems both from innovation and reflection. Each part of the RFQ connects to both aspects.

The Project Proposal is viewed largely as a method of reflection. This allows the team to look back on the project and figure out what could be done better. By doing this, year after year, the team has increasingly added value to each Project Proposal that is written. Each new paper reflects the previous year and contains instrumental differences that make the new paper more thoughtful than the last.

The team also considers the Prototype Display as a reflection of the value of the prototype, *Card Shark*. It is through the display that the innovative aspects of the canoe can be seen. This is done with the cross section, showing a posttensioning system, and the various materials samples stationed at the display. The theme is also emphasized in the creation of the display, showcasing a more artistic side of the team.

The Technical Presentation, essentially, is a condensed version of the Project Proposal. The team sees fit to highlight the most important details to add the most value to the presentation. This means that construction processes and material testing sections had to be shortened. The presentation that the team delivers is not unlike any other presentation an engineer might give in a design meeting. Overall, the visuals employed in the presentation are used to reflect the value of the prototype, along with any questions that are answered.

During the Prototype Performance Demonstration, each innovation made during the construction process is put to the test. The Demonstration is an integral part of the process and a culmination of the work put in throughout the year to produce a functional prototype. This year, the team focused on hull design and structural integrity. These core changes are seen as valuable because they reflect previous boats, but also innovative as they improve on previous designs. Overall, the team focused on innovating their practices from construction to management. At the start of the school year, Michigan Tech knew they wanted to implement a post-tensioning system in their prototype. The team spent the fall semester testing and designing a working system. Value lies in the integrity of the innovation. This meant testing needed to be comprehensive. The team met this goal through two main practice sessions when opposing end caps of the prototype were constructed with possible systems. The end caps were allowed to cure and then tested for strength later. At first, cables from previous years were used, but the team decided these were too large to fit in between the layers. A smaller cable diameter is used in the final boat.

Hull design was also a big part of the innovations made this year. *Kraken*, 2022's prototype, struggled with straight-line tracking. The hull design lead decided to create a prototype model that is both wider and has a keel. The thought behind this being that the boat would perform better in the sprint and co-ed races.

new Α curing tent was constructed to cure the prototype more efficiently. In previous years, a rudimentary tarp was hung approximately seven feet over the The new mold. tarp is hung over a four-foot-tall wooden-rafter style structure. This difference in

height creates a much

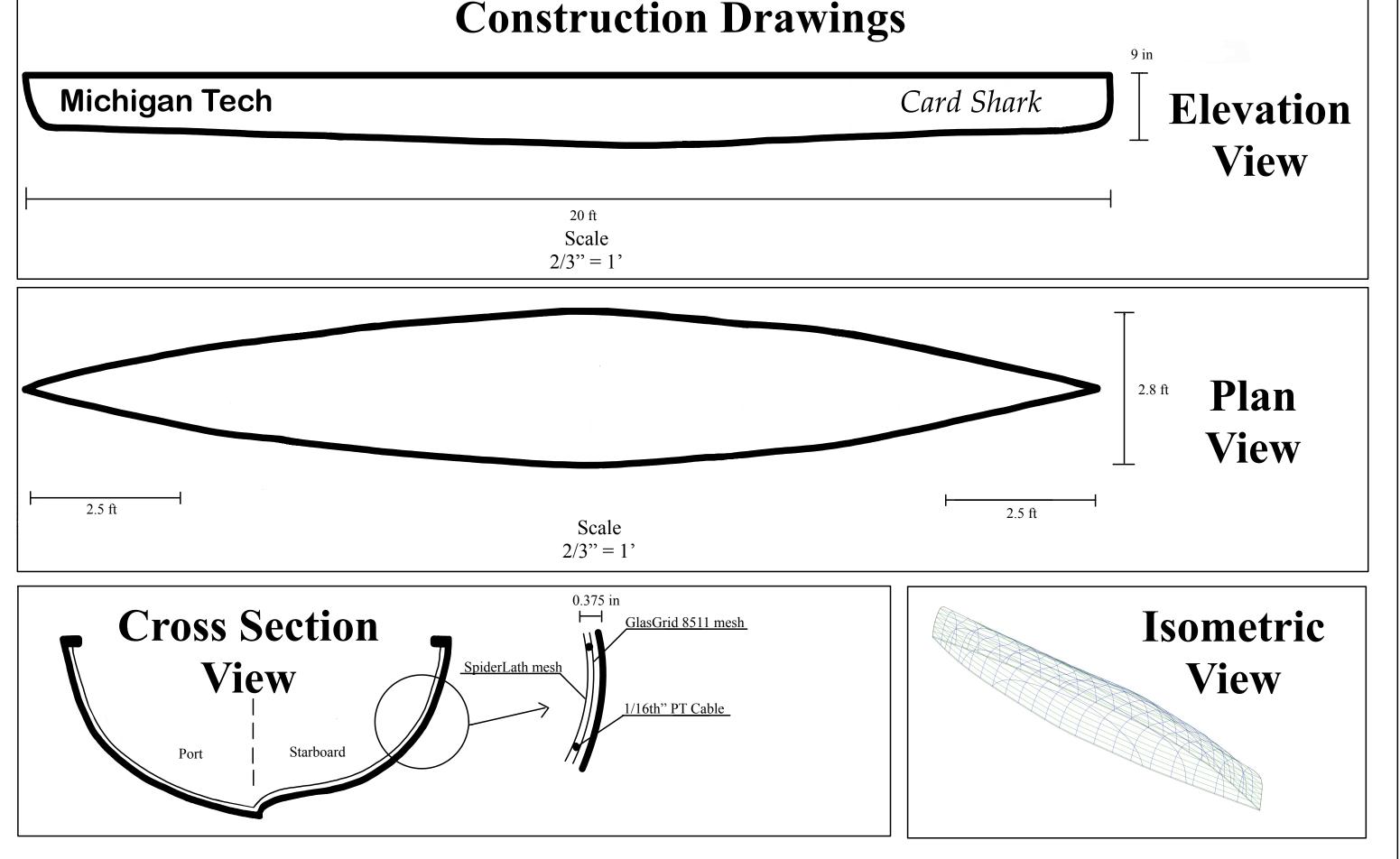


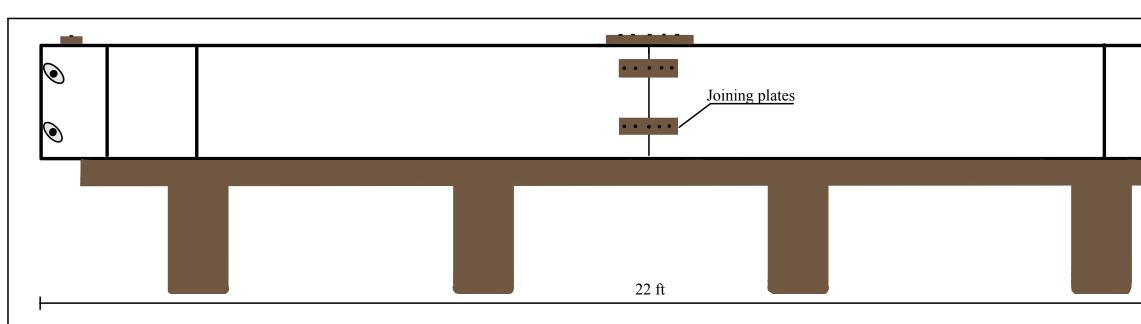
Figure 12: Curing tent structure without tarp

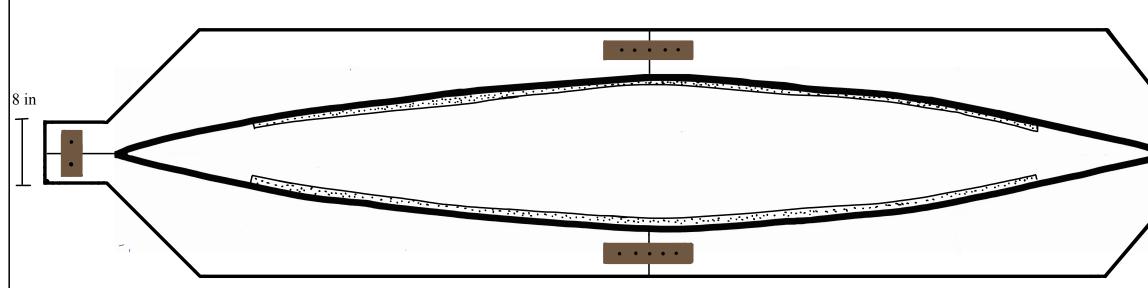
smaller curing environment. In turn, the team can sustain a 95% humidity level with less humidifiers than previous years required. In addition to the tent, ultrasonic humidifiers were primarily used to maintain a higher relative humidity within the curing tent compared to conventional humidifiers.

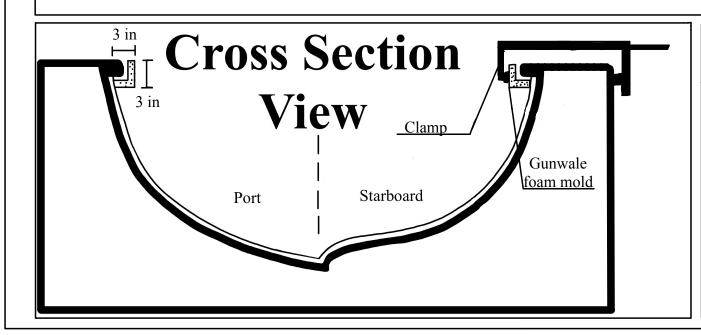


Construction Drawings





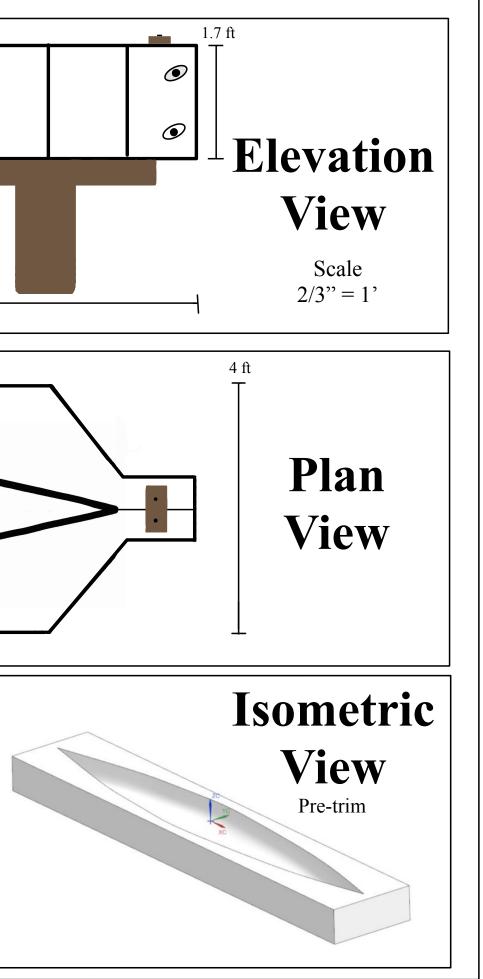




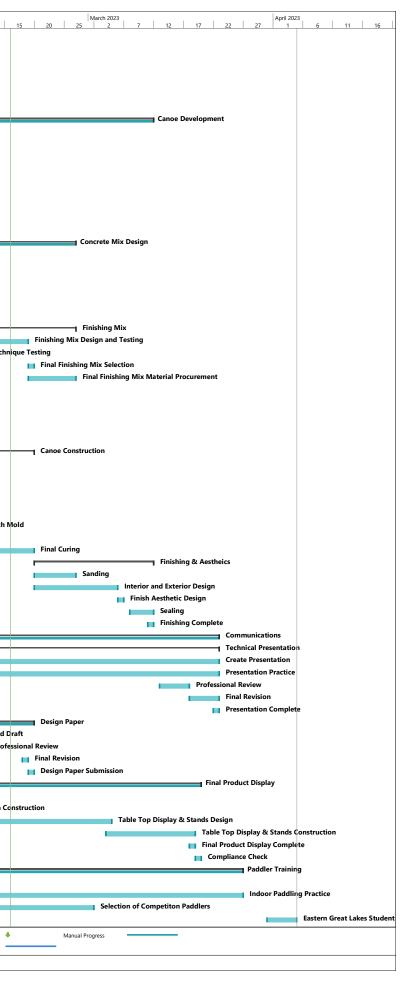
Michigan Tech

Card Shark Drawn by: Lydia Lamey Checked by: Max Hazen

Job: 2023 Card Shark



D 14	September 2022 October 2022 November 2022 December 2022 January 2023 9 24 29 3 8 13 18 23 28 2 7 12 17 22 27 2 7 12 17 22 27 1 6	February 2023
1	Project management	
2 3	Start of Academic Year Fundraising Fall News Letter	
4	Recruitment	
5	Lab Safety Training	
6	II Rules Released and Reviewed	
7	Theme Decision	
8 9	Hull Design	
10	Hull Design Research	
11	Draft of Initial Hull Design	
12	Rework of Hull Design	
13 14	 Final Hull Design Selection Release Hull Dimensions 	
15	Structural Analysis	
16	Foam Sized and CNC Milled	
17 18	Mold Pick-up and Delivery	
19	Material Procurement	
20	Structural Mix	
21	Binder,Aggregate,and Fiber Testing	
22 23	Final Structural Mix Selection	
23	Final Mix Testing Final Mix Testing	
25		F
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27 28		Application Tech
29		
30	r Reinforcement	
31	Material Procurement for Testing	
32 33	Reinforcement Testing Final Reinforcement Selection	
34	Final Reinforcement Material Procurement	
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36	Mold Assembly	Casting Practices
37 38	who assentially	Pre-batch Final Structural Mix
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70	Outdoor Paddling Practice	
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Project: Project Schedule Date: Thu 2/16/23	Task Milestone Project Summary Inactive Milestone Manual Task Manual Summary Rollup Start-only C Split Summary Inactive Task Inactive Summary Duration-only Manual Summary Finish-only 3	External Tasks Deadline External Milestone \diamond Progress
	Page 1	···



CARD SHARK ** * * * * *

Appendix A- Mixture proportions and calculations

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Appendix B- Mixture Proportions and Primary Mixture Calculation

MIXTURE: Primary Structural Mix

Introlte: I find y of dotard		CE	ME	NTITIC	DUS MA	TERIA	LS					
Component		Spe		Gravity		lume			Amount of C	M		
Portland Cement Type 1, c			3.15		1.15			$226.77 \ lb/yd^3$	Total		(in aludar a)	
Blast Furnace Slag, cm1			2.99		0.75			140.75 lb/yd ³		Total cm (includes c) 781.96 lb/yd ³		
Fly Ash - Class C, cm2			2.75			139 ft ³		195.49 lb/yd ³		c/cm ratio, by mass		
		2.22			$016 ft^3$		140.75 lb/yd ³		<u>0.29</u>			
Metakaolin, cm4						$570ft^3$		78.20 lb/yd ³				
					BERS							
Component		Spe	cific Gravity Volume						mount of Fib		4 7741	
Nycon PVA RF4000, fi						$5 ft^3$		$5.26 \ lb/yd^3$		Total Amount of Fibers <u>13.14</u> lb/yd ³		
Nycon PVA RFS400, f2					0.09	v		7.88 lb/yd ³		<u>13.1</u> 2	<u>•</u> 10/ya*	
				AGGR	EGATE	N I		Base Que	antity W		Volume,	
Aggregates			A	bs (%)	SGOD	SGss.	D	W oD	Wssd		Volume, Vagg, SSD	
Poraver 1 mm -2 mm, agg1				20 %	0.39	0.46	8	178.95 lb/yd ³	214.74 lb/y	d^3	7.350 ft^3	
Poraver .5 mm -1 mm, agg2			_	25 %	0.47	0.587		143.16 lb/yd ³	178.95 lb/y		$\frac{7.330 \text{ ft}^3}{4.880 \text{ ft}^3}$	
Poraver .25 mm5 mm, agg3			_	30 %	0.59	0.762		$25.56 \ lb/yd^3$	33.23 lb/yc		0.694 ft^3	
Poraver .1 mm3 mm, agg4				35%	0.90	0.796		$51.13 \ lb/yd^3$	69.03 lb/yc	_	0.910 ft^3	
K1 , agg ⁵				7.2 %	0.125	0.134	_	$10.23 \ lb/yd^3$	10.23 lb/yc		1.312 ft^3	
K37, agg6			_	6.8 %	0.37	0.39	5	5.11 lb/yd^3	5.11 lb/yd		$0.221 ft^3$	
Hess Pumice #3, agg7				16 %	0.769	0.892		$46.02 \ lb/yd^3$	53.38 lb/yc		$0.959 ft^3$	
Hess Pumice #5, agg8				17 %	0.737	0.8623		25.56 lb/yd ³	29.91 lb/yc		$0.556 ft^3$	
Hess Pumice #7, agg9				18 %	0.737	0.8679		25.56 lb/yd ³	$30.16 \ lb/yd^3$		$0.556 ft^3$	
			LIC	DUID A	DMIXT	TURES						
Admixture	lb/ US	gal	Do	sage ; / cwt)	% So			Amount of Water in Admixture				
MasterGlenium 7500, admx1	8.70	5		8	26	26 %		168 lb/yd ³		Total Water from		
MasterSet DEVLVO, admx2	8.97	7		6	54	76	3.124 lb/yd ³			Liquid Admixtures, $\sum w_{admx}$		
musici Sti DE (E) O, aumz				-				-	_(<u>6.291_lb/yd³</u>		
	50				DERE	_	IXТ					
Component		Spec		Gravity	Volun	<i>lume (ft³)</i> Amount (<i>lb/yd³</i>)				lide S		
Concrete Pigment, S_p			4.70	.70 $0 ft^3$		ft^3 0 lb/yd^3		Total Solids. Stotal 0 lb/yd ³				
				W	ATER					Ŭ		
						Amo	unt			Va	lume	
<i>Water,</i> w , $[=\Sigma (w_{free} + w_{admx} + w_{batc})$.)]				natio has		uni	297.14 lb/yd ³		$\frac{1}{4.762} ft^3$		
Total Free Water from All Aggres		free		w/c ratio, by mass 1.31			$-114.54 \ lb/yd^3$., 02	Ji	
Total Water from All Admixtures	o / ·	,		w/cm	<i>ratio</i> , by	mass	$6.29 \ lb/yd^3$					
Batch Water, Wbatch	· · · ·				0.38		4	05.39 lb/yd ³				
	DENSI	TIES, A	IR	CONTI	ENT, R	ATIOS		ND SLUMP				
Values for 1 cy of concre		cn			bers	Aggreg (SSD)	ate	Solids, Stotal	Water, v	v	Total	
Mass, M		781.96	lb	13.14	4 lb	625.82		0 lb	297.14 lb	2	EM:1718.07 lb	
Absolute Volume, V		4.633		0.162	<i>v</i>	17.44 f		$0 ft^3$	$4.762ft^3$		$\Sigma V:26.98 \ ft^3$	
Theoretical Density , T , $(=\Sigma M / \Sigma)$	(V)			lb/ft ³				<i>ir</i> , $[=(T-D)/T$			-1.6 %	
Measured Density, D			64.7	0				<i>Air</i> , $[= (27 - \Sigma V)$		_	0.085 %	
Total Aggregate Ratio ¹ (= $V_{agg.SSD}$ /27) 6				52 %		Slump, S	lum	p flow, Spread (as applicable	e)	1 in.	



MIXTURE: Secondary Structural Mix

MIXTORE. Secondary Struct		CF	ME	NTITIC	DUS M	ATERL	ALS				
Component				Gravity		lume			Amount	of CM	
Portland Cement Type 1, c			3.15		1.15	$54 ft^3$		226.77 lb/yd ³			<i></i>
,			2.99		0.75	v		140.75 lb/yd ³	$Total \ cm \ (includes \ c)$,
Fly Ash - Class C, cm22.			2.75			$39ft^3$		195.49 lb/yd ³	<u>781.96</u> lb/yd ³ c/cm ratio, by mass		
Silica Fume, cm3			2.22			$16 ft^3$		$140.75 \ lb/yd^3$ 0.29).29	
Metakaolin, cm4			2.2		0.52	$70ft^3$		78.20 lb/yd ³		-	
				FI	BERS						
Component		Spe	cific (Gravity		lume				of Fibers	
Nycon PVA RF4000, fi			1.3			$55 ft^3$		$5.26 \ lb/yd^3$,		ount of Fibers
Nycon PVA RFS400, f2			1.3			$97ft^3$		7.88 lb/yd ³		<u>13.</u>	<u>14</u> lb/yd ³
				Aggr	EGATI	ES					
Aggregates			A	bs (%)	SGOD	SGss	SD	Base Que			Volume,
								W OD		SSD	Vagg, SSD
Poraver 1 mm -2 mm, agg1			_	20 % 25 %	0.39 0.47	0.46		$195.12 \ lb/yd^3$		$4 lb/yd^3$	$8.018 ft^3$
Poraver .5 mm -1 mm, agg2			_	23 % 30 %	0.47	0.38		$\frac{0 \ lb/yd^3}{88.60 \ lb.6.4^3}$		$\frac{b}{yd^3}$	$0 ft^3$
<i>Poraver .25 mm5 mm, agg3</i> <i>Poraver .1 mm3 mm, agg4</i>			_	30 % 35%	0.39	0.79		88.69 lb/yd ³ 29.56 lb/yd ³		0 lb/yd ³ ' lb/yd ³	$\frac{2.409 ft^3}{0.526 ft^3}$
K1, agg ⁵			_	55% 7.2 %	0.30	0.13		$\frac{29.36 lb/ya^2}{0 lb/yd^3}$		b/yd ³	$\frac{0.326 \text{ft}}{0 \text{ft}^3}$
K37, agg6			_	6.8 %	0.125	0.13		$\frac{0.107ya}{23.65 lb/yd^3}$		5 lb/yd ³	$\frac{0 ft}{1.024 ft^3}$
Hess Pumice #3, agg7			_	16 %	0.769	0.89		$\frac{23.05 \ lb/yd}{70.95 \ lb/yd^3}$		$\frac{10}{ya}$	1.024 ft 1.479 ft^3
Hess Pumice #5, agg			_	10 % 17 %	0.737	0.862		$\frac{100.52 lb/yd^3}{100.52 lb/yd^3}$		$0 \ lb/yd^3$	$2.186 ft^3$
Hess Pumice #7, aggs			_	18 %	0.737	0.862		82.78 <i>lb/yd</i> ³		$\frac{0}{10/yd^3}$	$\frac{2.100 \text{ ft}}{1.800 \text{ ft}^3}$
11055 1 411100 11 1, 4887						ΓURES	-	02.70 <i>lory</i> a	77.00	, <i>101</i> ya	1.000 Ji
				sage							
Admixture	lb/US	gal		/ cwt)	% S	olids		Amount	of Wate	er in Adn	nixture
MasterGlenium 7500, admx1	8.76			8	26	26 % 3		3.168 lb/yd ³			Water from
MasterSet DEVLVO, admx2	8.97	,		6	5			2.124 lb/yd ³	— Lie		<i>iixtures</i> , ∑wadmx
Musier Sei DE V EVO, aumaz				×				•		_6.2	<u>91_</u> lb/yd ³
	SO	<u> </u>					IXT	'URES)		2	
Component		Spec	<mark>eific</mark> G	aravity	Volui	ne (ft ³)		$Amount (lb/yd^3)$			a 1: 1 a
Concrete Pigment, S_p			4.70		0	ft ³		$0 \ lb/yd^3$		lotal i 0	Solids. Stotal lb/yd ³
				XX/	ATER					0	107 yu
				V V	AIEK	4				T	olume
Wedge E. S. () 1					Amo	Junt	207.14.11.4.13			
Water, w, $[=\sum (w_{free} + w_{admx} + w_{batc})$ Total Free Water from All Aggres			_	w/c	ratio, by	mass	1	<u>297.14 lb/yd³</u> 20.93 lb/yd ³		4.70	$52 ft^3$
Total Water from All Admixtures		ree		w/cm	<u>1.31</u> 1 ratio, b	v mass	-1.	6.29 <i>lb/yd</i>			
Batch Water, Wbatch	, _, ~, ~, ~, ~, ~, ~, ~, ~, ~, ~, ~, ~, ~,		-		<u>0.38</u>	, 110055	4	12.78 lb/yd ³			
	DENSU	TTES A	TP	CONT	ENT L			ND SLUMP			
Values for 1 cy of concre		cm			bers	Aggre	gate	Solids, Stotal	W	ater, w	Total
Mass, M		781.96	lb	13.14	4 lb	712.19	/	0 lb	297.	.14 lb	∑M:1804.43 lb
Absolute Volume, V		4.633 j		0.162		17.44 j				$52 ft^3$	$\Sigma V:26.98 \ ft^3$
Theoretical Density , T, $(=\Sigma M / \Sigma)$	(V)	0	66.88	lb/ft ³	1	Air Cont	e <mark>nt,</mark> A	Air, $[= (T - D)/T$	$[=(T-D)/T \times 100\%]$		1.02 %
Measured Density, D			66.2	lb/ft ³				<i>Air</i> , $[= (27 - \Sigma V)$			0.08 %
Total Aggregate Ratio ¹ (= $V_{age,SSD}$ /	27)		64.5	2 %		Slump, S	Slum	p flow, Spread (as appl	icable)	1 in.



MIXTURE: Finishing Mix

		CF	MF	NTITIC	M SII	ATERIA	AT S				
				Gravity		lume			Amou	ent of CM	
	Portland Cement Type 1, c 3.1					33 ft^3		153.86 lb/yd ³			
Blast Furnace Slag, cmi			2.99			17 ft^3		230.79 lb/yd ³	Total cm (include		
Fly Ash - Class C, cm2 2.1			2.75			$\frac{1}{1000}$ $\frac{1}{1000}$ $\frac{1}{1000}$		153.86 lb/yd ³	\sim		$31 lb/yd^3$
Silica Fume, cm3			2.22	$22 0 ft^3$		$0 \ lb/yd^3$	c/cm ratio, by mass				
Metakaolin, cm4			2.2		1.68	$BI ft^3$		230.79 lb/yd ³	<u>0.20</u>		<u>,,20</u>
				FI	BERS						
Component		Spe	cific (Gravity	Va	lume		A	moun	t of Fibers	
Nycon PVA RF4000, fi			1.3			ft ³		$0 \ lb/yd^3$			ount of Fibers
Nycon PVA RFS400, f2			1.3		0.05	$54 ft^3$		4.38 lb/yd ³		<u>4.3</u>	<u>8_</u> lb/yd ³
				AGGR	EGATI	ES					
Aggregates			A	bs (%)	SGOD	SGss	ית <i>ו</i>	Base Que	antity		Volume,
								W OD		WSSD	Vagg, SSD
Poraver 1 mm -2 mm, agg1				20 %	0.39	0.46		$\frac{0 \ lb/yd^3}{2}$	<u> </u>	$\frac{1}{b/yd^3}$	$0 ft^3$
Poraver .5 mm -1 mm, agg2				25 %	0.47	0.587		$0 lb/yd^3$) lb/yd^3	$0ft^3$
Poraver .25 mm5 mm, agg3			+	30 %	0.59	0.76		$149.00 \ lb/yd^3$		$\frac{1.70 \ lb/yd^3}{22}$	$4.047 ft^3$
Poraver .1 mm3 mm, agg4			_	35%	0.90	0.796		$164.68 \ lb/yd^3$.32 lb/yd ³	$2.932 ft^3$
K1, agg5			_	7.2 %	0.125	0.13		$0 lb/yd^3$) lb/yd^3	$0 ft^3$
K37 , agg6				6.8 %	0.37	0.39		$15.68 \ lb/yd^3$		$75 \ lb/yd^3$	$0.679 ft^3$
Hess Pumice #3, agg7			_	16 %	0.769	0.89		$149.00 \ lb/yd^3$	-	$\frac{1.84 \text{ lb/yd}^3}{1.84 \text{ lb/yd}^3}$	$3.106 ft^3$
Hess Pumice #5, agg8			_	17 %	0.737	0.862		$149.00 \ lb/yd^3$		$\frac{1.33 \text{ lb/yd}^3}{1.33 \text{ lb/yd}^3}$	$3.191 ft^3$
Hess Pumice #7, agg9				18 %	0.737	0.867	/9	156.84 lb/yd ³	185	$1.07 \ lb/yd^3$	$3.411ft^3$
				QUID A	DMIX	ΓURES					
Admixture	lb/ US	gal		sage ; / cwt)	% S	olids	ds Amount of Water in Admixture				nixture
MasterGlenium 7500, admx1	8.76	5		8	26	26 %		,, iorya		Water from	
MasterSet DEVLVO, admx2	8.97	7		0	5	%	$0 \ lb/yd^3$		^	Liquid Admixtures, ∑wadmx _3.117_lb/yd ³	
	So		WF	S POW	DEBE.	DADM	ТУТ	TIBES)			<u></u>
Component	50	l l		Gravity		ne (ft ³)		,	ทอบท	t (] h/vd ³)	
		Spec						Amount (lb/yd ³) Total Solids. S			Solids. Stotal
Concrete Pigment , Sp			4.70		0.01	$7 ft^3$		$5 lb/yd^3$		5	
				W	ATER						
						Amo	ount			V	olume
Water, w, $[=\Sigma (w_{free} + w_{admx} + w_{batc})]$	ı) <i>1</i>			wle	ratio, by			307.73 lb/yd ³			$1 ft^3$
Total Free Water from All Aggres		free		Wit	<u>2.0</u>	mass	-10	$80.81 \ lb/yd^3$			5
Total Water from All Admixtures				w/cm	ratio, b	v mass		$3.12 \ lb/yd^3$			
Batch Water, Wbatch				-	0.4		4	85.56 lb/yd ³			
	DENSI	fies, A	IR	CONT	ent, F	ATIOS	, Al	ND SLUMP			
Values for 1 cy of concre	ete	ст	ļ	Fil	bers	Aggreg (SSD		Solids, Stotal		Water, w	Total
Mass, M		769.31	lb	4.38	lb	965.01	/			07.73 lb	∑M2051.43 lb
Absolute Volume, V		4.598 j	ť	0.054	$4 ft^3$	17.37 f	t ³	$0.017ft^3$	4.	931 ft ³	$\Sigma V:26.97 \ ft^3$
Theoretical Density , T, $(=\Sigma M / \Sigma)$	<i>V</i>)	(lb/ft ³	1	Air Content, Air, $[=(T-D)/T \times 1]$			'x 10	0%]	-2.12 %
Measured Density, D				lb/ft ³				<i>Air</i> , $[= (27 - \Sigma V)$			0.11 %
Total Aggregate Ratio ¹ (= $V_{age,SSD}$ /	27)		64.5	52 %		Slump, S	Slum	p flow, Spread (as ap	plicable)	1.5 in.



CARD SHARK ** * * * * *

Cementitious Materials

Mass= Given SG= Given Volume= Mass/(SG*62.4 lbs/ft³)

Portland Cement

 $\label{eq:Greense} \begin{array}{l} Mass_{\rm Pc} = 226.77 \ lbs \\ SG_{\rm Pc} = 3.15 \\ VPC = 226.77 \ lbs \\ 3.15*62.4 \ lbs / ft \\ 3 = 1.154 \ ft \\ \end{array}$

Blast Furnace Slag Mass_{BFS}= 140.75 lbs SG_{RFS} = 2.99

VBFS=140.75 lbs2.99*62.4 lbs/ft3=0.754 ft3

Fly Ash Class C

 $\begin{array}{l} Mass_{\mbox{\tiny FA}}{=}\ 195.49 \ lbs\\ SG_{\mbox{\tiny FA}}{=}\ 2.75\\ VFA{=}195.49 \ lbs 2.75{*}62.4 \ lbs/ft 3{=}1.139 \ ft 3 \end{array}$

Undensified Silica Fume $Mass_{sr}= 140.75 lbs$ $SG_{sr}= 2.22$ VSF=140.75 lbs2.22*62.4 lbs/ft3=1.016 ft3

Metakaolin Mass_{MK}= 78.20 lbs

 SG_{MK} = 2.20 VMK=78.20 lbs2.20*62.4 lbs/ft3=0.570 ft3

 Σ Mass_{Cementitious}= 781.96 lbs Σ Volume _{Cementitious}= 4.633 ft³

 $C/CM = Mass_{PC} / \Sigma Mass_{Cementitious} = 0.29$

Fibers

Mass= Given SG= Given Volume= Mass/(SG*62.4 lbs/ft³)

 $\begin{array}{l} Mass_{\text{RF}} = 5.26 \ lbs \\ SG_{\text{RF}} = 1.3 \\ VRF = 5.26 \ lbs 1.3*62.4 \ lbs/ft 3 = 0.065 \ ft 3 \end{array}$

 $Mass_{RFS} = 7.88 \ lbs$



CARD SHARK 🐂 🐂 🐂 🐂 🐂

SG_{RFS}= 1.3 VRFS=7.88 lbs1.3*62.4 lbs/ft3=0.097 ft3

 Σ Mass_{fibers}= 13.14 lbs Σ Volume_{fibers}= 0.162 ft³

Aggregates

Mass (W_{oD})= Given SG_{oD}= Given Absorption(Abs)= Given Mass (W_{STK})= Given Mass (W_{SSD})= (1+ Abs/100)* W_{oD} SG_{SSD}=(1+ Abs/100)*SG_{oD} Volume= $W_{SSD}/(SG_{SSD}*62.4 \text{ lbs/ft}^3)$ MC_{TOTAL}= (($W_{STK}-W_{OD}/W_{OD}$)*100 MC_{FREE}= MC_{Total}-Abs W_{FREE} = W_{OD} * (MC_{FREE}/100)

Poraver 1 mm- 2 mm

$$\begin{split} W_{\text{ODp1-2}} &= 178.95 \text{ lbs} \\ SG_{\text{ODp1-2}} &= 0.39 \\ Abs_{\text{p1-2}} &= 20\% \\ W_{\text{STKp1-2}} &= 178.95 \text{ lbs} \\ W_{\text{SSDp1-2}} &= (1+(20/100))*178.95 = 214.74 \text{ lbs} \\ SG_{\text{SSDp1-2}} &= (1+(20/100))*0.39 = 0.468 \\ V_{\text{SSDp1-2}} &= 214.74 \text{ lbs} 0.468*62.4 \text{ lbs/ft3} = 7.35 \text{ ft3} \\ MC_{\text{TOTAL,p1-2}} &= ((178.95-178.95)/178.95)*100 = 0\% \\ MC_{\text{FREEp1-2}} &= 0\%-20\% = -20\% \\ W_{\text{FREEp1-2}} &= 178.95*(-20\%/100) = -35.79 \text{ lbs} \end{split}$$

Poraver 0.5 mm-1 mm

$$\begin{split} W_{\text{ODp0.5-1}} &= 143.16 \text{ lbs} \\ SG_{\text{ODp0.5-1}} &= 0.47 \\ Abs_{\text{p0.5-1}} &= 25\% \\ W_{\text{STK,p0.5-1}} &= 143.16 \text{ lbs} \\ W_{\text{STK,p0.5-1}} &= (1+(25/100))*143.16 = 178.95 \text{ lbs} \\ SG_{\text{SSD,p0.5-1}} &= (1+(25/100))*0.47 = 0.5875 \\ V_{\text{SSD,p0.5-1}} &= 178.95 \text{ lbs}0.5875*62.4 \text{ lbs/ft3} = 4.88 \text{ ft3} \\ MC_{\text{TOTAL,p0.5-1}} &= ((173.16-143.16)/143.16)*100 = 0\% \\ MC_{\text{FREEp0.5-1}} &= 0\%-25\% = -25\% \\ W_{\text{FREEp0.5-1}} &= 143.16*(-25\%/100) = -35.79 \text{ lbs} \end{split}$$

Poraver 0.25 mm-0.5mm

 $W_{\text{ODp0.25-0.5}} = 25.56 \ lbs \\ SG_{\text{ODp0.25-0.5}} = 0.59$





$$\begin{split} Abs_{p025.0.5} &= 30\% \\ W_{\text{STKp025-0.5}} &= 25.56 \text{ lbs} \\ W_{\text{SDp025-0.5}} &= (1+(30/100))*25.56 = 33.228 \text{ lbs} \\ \text{SG}_{\text{SSDp025-0.5}} &= (1+(30/100))*0.59 = 0.767 \\ V_{\text{SSDp025-0.5}} &= 33.228 \text{ lbs}0.767*62.4 \text{ lbs/ft3} = 0.6943 \text{ ft3} \\ \text{MC}_{\text{TOTALp025-0.5}} &= ((25.56-25.56)/25.56)*100 = 0\% \\ \text{MC}_{\text{FREEp025-0.5}} &= 0\% - 30\% \\ W_{\text{FREEp025-0.5}} &= 25.56*(-30\%/100) = -7.668 \text{ lbs} \end{split}$$

Poraver 0.1 mm- 0.3 mm

$$\begin{split} W_{\text{ODp0.1-0.3}} &= 51.13 \text{ lbs} \\ SG_{\text{ODp0.1-0.3}} &= 0.90 \\ Abs_{\text{p0.1-0.3}} &= 35\% \\ W_{\text{STKp0.1-0.3}} &= 51.13 \text{ lbs} \\ W_{\text{SSDp0.1-0.3}} &= (1+(35/100))*51.13 = 69.0255 \text{ lbs} \\ SG_{\text{SSDp0.1-0.3}} &= (1+(35/100))*0.90 = 1.215 \\ V_{\text{SSDp0.1-0.3}} &= 69.0255 \text{ lbs}1.215*62.4 \text{ lbs/ft3} = 0.9104 \text{ ft3} \\ MC_{\text{TOTALp0.1-0.3}} &= ((51.13-51.13)/51.13)*100 = 0\% \\ MC_{\text{FREEp0.1-0.3}} &= 0\%-35\% \\ W_{\text{FREEp0.1-0.3}} &= 51.13*(-35\%/100) = -17.896 \text{ lbs} \end{split}$$

K1

$$\begin{split} W_{\text{ODKI}} &= 10.23 \text{ lbs} \\ SG_{\text{ODKI}} &= 0.125 \\ Abs_{\text{ODKI}} &= 7.2\% \\ W_{\text{STKKI}} &= 10.23 \text{ lbs} \\ W_{\text{SSDKI}} &= (1+(7.2/100))*10.23 = 10.967 \text{ lbs} \\ SG_{\text{SSDKI}} &= (1+(7.2/100))*0.125 = 0.134 \\ V_{\text{SSDKI}} &= 10.967 \text{ lbs} 0.134*62.4 \text{ lbs/ft3} = 1.3116 \text{ ft3} \\ MC_{\text{TOTAL KI}} &= ((10.23-10.23)/10.23)*100 = 0 \% \\ MC_{\text{FREE KI}} &= 0\%-7.2\% = -7.2\% \\ W_{\text{FREE KI}} &= 10.23*(7.2\%/100) = -0.737 \text{ lbs} \end{split}$$

K37

$$\begin{split} W_{\text{ODK37}} &= 5.11 \text{ lbs} \\ SG_{\text{ODK37}} &= 0.37 \\ Abs_{\text{ODK37}} &= 6.8\% \\ W_{\text{STK37}} &= 5.11 \text{ lbs} \\ W_{\text{STK437}} &= 5.11 \text{ lbs} \\ W_{\text{SSDK37}} &= (1 + (6.8/100)) * 5.11 = 5.46 \text{ lbs} \\ SG_{\text{SSDK37}} &= (1 + (6.8/100)) * 0.37 = 0.395 \\ V_{\text{SSDK37}} &= 5.46 \text{ lbs} 0.395 * 62.4 \text{ lbs/ft3} = 0.2215 \text{ ft3} \\ MC_{\text{TOTAL K37}} &= ((5.11 - 5.11)/5.11) * 100 = 0\% \\ MC_{\text{FREE K37}} &= 0\% - 6.8\% \\ W_{\text{FREE K37}} &= 5.11 * (6.8\%/100) = -0.347 \text{ lbs} \end{split}$$

Hess Pumice #3





$$\begin{split} W_{\text{ODp#3}} &= 46.02 \text{ lbs} \\ SG_{\text{ODp#3}} &= 0.769 \\ Abs_{\text{ODp#3}} &= 16\% \\ W_{\text{STKp#3}} &= 46.02 \text{ lbs} \\ W_{\text{SSDp#3}} &= (1 + (16/100))^* 49.02 = 53.3832 \text{ lbs} \\ SG_{\text{SSDp#3}} &= (1 + (16/100))^* 0.769 = 0.892 \\ V_{\text{SSDp#3}} &= 53.3832 \text{ lbs} 0.892^* 62.4 \text{ lbs/ft3} = 0.9591 \text{ ft3} \\ MC_{\text{TOTALp#3}} & ((46.02 - 46.02)/46.02)^* 100 = 0\% \\ MC_{\text{FREEp#3}} &= 0\% - 16\% = -16\% \\ W_{\text{FREEp#3}} &= 46.02^* (-16\%/100) = -7.36 \text{ lbs} \end{split}$$

Hess Pumice #5

$$\begin{split} W_{\text{ODp#S}} &= 25.56 \text{ lbs} \\ SG_{\text{ODp#S}} &= 0.737 \\ Abs_{\text{ODp#S}} &= 17\% \\ W_{\text{STKp#S}} &= 25.56 \text{ lbs} \\ W_{\text{SSDp#S}} &= (1+(17/100))*25.56 = 29.9052 \text{ lbs} \\ SG_{\text{SSDp#S}} &= (1+(17/100))*0.737 = 0.8623 \\ V_{\text{SSDp#S}} &= 29.9052 \text{ lbs}0.8623*62.4 \text{ lbs/ft3} = 0.5558 \text{ ft3} \\ MC_{\text{TOTALp#S}} &= ((25.56-25.56)/25.56)*100 = 0\% \\ MC_{\text{FREEp#S}} &= 0\% - 17\% = -17\% \\ W_{\text{FREEp#S}} &= 25.56*(-17\%/100) = -4.35 \text{ lbs} \end{split}$$

Hess Pumice #7

$$\begin{split} & W_{\text{ODp#7}} = 25.56 \text{ lbs} \\ & SG_{\text{ODp#7}} = 0.737 \\ & Abs_{\text{ODp#7}} = 18\% \\ & W_{\text{STKp#7}} = 25.56 \text{ lbs} \\ & W_{\text{SSDp#7}} = (1+(18/100))*25.56 = 30.1608 \text{ lbs} \\ & SG_{\text{SSDp#7}} = (1+(18/100))*0.737 = 0.8697 \\ & V_{\text{SSDp#7}} = 30.1608 \text{ lbs}0.8697*62.4 \text{ lbs/ft3} = 0.5557 \text{ ft3} \\ & MC_{\text{TOTALp#7}} = ((25.56-25.56)/25.56)*100 = 0\% \\ & MC_{\text{FREEp#7}} = 0\% - 18\% = -18\% \\ & W_{\text{FREEp#7}} = 25.56*(-18\%/100) = -4.6 \text{ lbs} \end{split}$$

 Σ Mass_{Aggregates} = 625.82 lbs Σ Volume _{AggregatesSD} = 17.44 ft³ Σ W_{FREE} = -114.538 lbs

Admixtures

Dosage(D)= Given %Solids= Given Density(ρ)= Given Water Content (WC)= 100 - %Solids Water = Dosage * cwt * WC*(1/128)*Density





MasterGelenium 7500

$$\begin{split} D_{\rm MG7500} &= 8 \ fl \ oz/cwt \\ \rho_{\rm MG7500} &= 8.76 \ lb/Gal \\ \%S_{\rm MG7500} &= 26\% \\ \%WC_{\rm MG7500} &= 100\% - 26\% = 74\% \\ W_{\rm MG7500} &= 8*(781.96/100)*0.74*(1/128)*8.76 = 3.168 \ lbs \end{split}$$

MasterSet DELVO

 $\begin{array}{l} D_{\mbox{\tiny MSDELVO}} = \ 6 \ fl \ oz/cwt \\ \rho_{\mbox{\tiny MSDELVO}} = \ 8.97 \ lb/Gal \\ \% S_{\mbox{\tiny MSDELVO}} = \ 5\% \\ \% W C_{\mbox{\tiny MSDELVO}} = \ 100\% - \ 5\% = \ 95\% \\ W_{\mbox{\tiny MSDELVO}} = \ 6*(781.96/100)*0.95*(1/128)*8.97 = \ 3.124 \ lbs \end{array}$

$\Sigma W_{ADMX} = 6.291 \text{ lbs}$

Water

w/cm = 0.38 $M_{water} = M_{CM} * w/cm$ $V_{water} = (M_{water} / 62.4 \text{ lbs/ft}^3)$ $W_{BATCH} = M_{water} - (\Sigma W_{ADMX} + W_{FREE})$

$$\begin{split} M_{\text{water}} &= 781.96 * 0.38 = 297.14 \text{ lbs} \\ V_{\text{water}} &= 297.145/62.4 = 4.762 \text{ ft}^3 \\ W_{\text{BATCH}} &= 297.145 \text{ -} (6.291 \text{+} \text{-} 114.538) \text{=} 405.392 \text{ lbs} \end{split}$$

Concrete Analysis

 $\Sigma Mass_{Total} = 781.96 + 13.14 + 625.82 + 297.145 = 1718.065 \text{ lbs}$ $\Sigma Volume_{Total} = 4.633 + 0.162 + 17.44 + 4.762 = 26.977 \text{ ft}^3$ w/c = 297.145/226.77 = 1.31Theoretical Density: 1718.065/26.977 = 63.68 lb/ft³ Total Aggregate Ratio: 17.44/27 *100 = 64.59 % OK Air content: ((63.68-64.7)/63.68) *100 = -1.6 % Air content: ((27-26.977)/27) *100 = 0.085 %



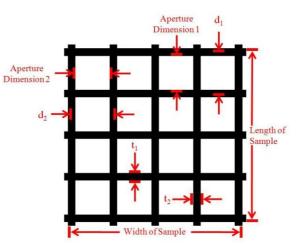
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Appendix C- Hull Thickness/Reinforcement and Percent Open Area Calculations

Percent Open Area Calculations

Samples: SpiderLath(SL) and GlasGrid®8511(GL) Mesh

Given	
$N_{1,SL} = 34$	number of apertures along length
$N_{1,GG} = 9$	
$N_{2,SL} = 35$	number of apertures along width
$N_{2,GG} = 5$	
$T_{1,SL} = 0.103$ in	average thickness of reinforcement along length
$T_{1,GG} = 0.262$ in	
$T_{2,SL} = 0.051$ in	average thickness of reinforcement along width
$T_{2,GG} = 0.173$ in	



Average spacing of reinforcement

(center-to-center) along the sample

Average spacing of reinforcement

(center-to-center) along the sample

Area_{Total,SL} = 167.05 in^2 $Area_{Total,GG} = 1120 in^2$

length

width

Aperture	Dimension_	1_	SL = 0.312 in
Aperture	Dimension_	1	_GG= 0.737 in
Aperture	_Dimension_1	2	SL= 0.288 in
Aperture	_Dimension_1	2	_GG= 0.808 in

$D_1 = Aperture_$	Dimension_	1+2*(t1/2)
-------------------	------------	-------	-------

Dem

Lengt

Width

nonstrated Compliance	
$gth_{Sample} = N_1 * D_1$	Length _{SL} = 14.09 in Length _{GG} = 8.98 in
$th_{Sample} = N_2 * D_2$	Width _{SL} = 11.85 in Width _{GG} = 4.91 in

 $D_{1,SL} = 0.42$ in

 $D_{1,GG} = 0.99$ in

 $D_{2.SL} = 0.34$ in

 $D_{2,GG} = 0.98$ in

Area_{Open,SL} = 106.76 in^2 Area_{Open} = N_1 *n2*Aperture Dimension 1*Aperture Dimension 2 $Area_{Open,GG} = 680 \text{ in}^2$

Area_{Total} = Length_{Sample}*Width_{Sample}

 $POA = (Area_{Open}/Area_{Tota})*100$ POA _SL= 63.9% > 40% *Compliant* POA GG = 60.7% > 40% *Compliant*





Hull Thickness

Known Values

$$\begin{split} T_{G} &= 0.045 \text{ in} \\ T_{S} &= 0.050 \text{ in} \\ T_{C} &= 0.0625 \text{ in} \\ T_{H} &= 0.375 \text{ in} \end{split}$$

Average thickness of first layer of reinforcement, GlasGrid®8511 Mesh Average thickness of second layer of reinforcement, SpiderLath Mesh Thickness of PT cable Overall hull thickness

 $\frac{0.045in + 0.050in + 0.0625in}{0.375in} * 100\% = 42\%$

42% < 50% *Compliant*

Bow and Stern Thickness

Known Values	
$T_G = 0.045$ in	Average thickness of first layer of reinforcement, GlasGrid®8511 Mesh
$T_{\rm S} = 0.050$ in	Average thickness of second layer of reinforcement, SpiderLath Mesh
$T_{\rm H} = 0.500$ in	Nominal hull thickness in bow and stern

 $\frac{0.045in + 0.050in}{0.500 in} * 100\% = 19\%$ $\frac{19\%}{50\%} Compliant$

Gunwale Thickness

Known Values $T_G = 0.045$ in $T_W = 1$ in

Average thickness of gunwale reinforcement, GlasGrid®8511 Mesh Nominal thickness of gunwale rail

 $\frac{0.045in}{1in} * 100\% = 4.5\%$

4.5% < 50% *Compliant*

PT Anchor Thickness

Known Values	
$T_{\rm B} = 0.0359$ in	Thickness of bearing plate
$T_{\rm S} = 0.050$ in	Average thickness of reinforcement, SpiderLath Mesh
$T_{\rm C} = 0.0625$ in	Thickness of PT cable
$T_{PT} = 2$ in	Anchor concrete thickness

 $\frac{0.0359 \text{ in} + 0.050 \text{ in} + 0.0625 \text{ in}}{2 \text{ in}} * 100\% = 7.42\%$

7.42 % < 50 % *Compliant*

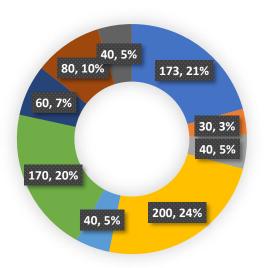




Appendix D- Detailed Fee Estimate

Role	Projected Person- Hours	Hourly Rate	Cost
Principle Design Engineer	100	\$50	\$5,000
Design Manager	68	\$45	\$3,060
Project Construction Manager	30	\$40	\$1,200
Construction Superintendent	75	\$40	\$3,000
Project Design Engineer	50	\$35	\$1,750
Quality Manager	42	\$35	\$1,470
Graduate Field Engineer	0	\$35	\$0
Technician Drafter	18	\$25	\$450
Laborer/Technician	425	\$25	\$10,625
Clerk/ Office Admin	30	\$15	\$450
Outside Consultants	10	\$200	\$2,000
Total	848 hours		\$29,005
		Labor costs with direct, indirect, and profit multipliers	\$115,439.90

Hourly Breakdown by Project



- Project Management
- Hull Design
- Structural Analysis
- Mixture Design Development
- Mold Construction
- Canoe Construction
- Project Proposal
- Presentation
- Display



CARD SHARK

Expenses

Material	Unit Cost	Amount Used	Net Cost
Type 1 Portland Cement C-150	\$0.26/lb	40.8 lbs	\$10.61
Blast Furnace Slag	\$0.08/lb	26.3 lbs	\$2.10
Fly Ash - Class C	\$0.02/lb	35.3 lbs	\$0.71
NORCHEM Undensified Silica Fume	\$0.04/lb	24.6 lbs	\$0.98
Metakaolin	\$1.10/lb	15.4 lbs	\$16.94
NYCON PVA RF4000	\$11.10/lb	1 lbs	\$11.10
NYCON PVA RFS400	\$11.00/lb	1.4 lbs	\$15.40
Poraver 1-2 mm	\$0.75/lb	29.5 lbs	\$22.13
Poraver 0.5-1 mm	\$0.75/lb	15.6 lbs	\$11.70
Poraver 0.25-0.5 mm	\$0.75/lb	11.5 lbs	\$8.63
Poraver 0.1-0.3 mm	\$0.75/lb	8.5 lbs	\$6.38
K1	\$14.78/lb	1.1 lbs	\$16.26
K37	\$9.40/lb	2.6 lbs	\$24.44
Pumice #3	\$0.70/lb	10.6 lbs	\$7.42
Pumice #5	\$0.67/lb	11.8 lbs	\$7.91
Pumice #7	\$0.67/lb	10.8 lbs	\$7.24
Pigment	\$7.99/lb	0.15 lbs	\$1.20
Water	\$0/gal	74.8 lbs	\$0.00
BASF MasterSet DELVO	\$22.60/gal	0.06 gal	\$1.36
BASF MasterGelenium 7500	\$53.34/gal	0.08 gal	\$4.26
GlasGrid® 8511 Mesh	\$2.51/ft ²	65 ft ²	\$163.15
SpiderLath Mesh	\$0.78/ft ²	65 ft ²	\$50.70
Steel Cable	\$0.29/ft	130 feet	\$37.70
Cable Sleeve	\$0.29/ft	130 feet	\$37.70
Bearing Plate	\$1.16/unit	1 unit	\$1.16
Wire Rope Stop	\$0.24/unit	6 units	\$1.44
Expanding Foam	\$124.99/2 gal kit	1 kit	\$124.99
Concrete Stain	\$444/ gal	.25 gal	\$111.00
Concrete Sealant	\$79.60/gal	2 gal	\$159.20

Total Cost: \$893.81 **With markup:** total cost * 1.10 = \$983.20

Lump sum fee for mold construction = material cost + transportation = \$500 + \$400 = \$900 Lump sum fee for transportation to Platteville, WI= gas + accommodations = \$500 + \$600 = \$1100 *using MTUCC trailer and members to drive*

Combined cost: Labor + Materials + Mold Construction + Transportation = 115,439.90 + 983.20 + 900 + 1100 = \$118,423.10





Appendix E: Supporting Documentation

November 4th, 2022

Michigan Technological University Concrete Canoe Team Grover C. Dillman Hall 1700 Townsend Drive Houghton, Michigan 49931

To: ASCE Student Services 1801 Alexander Bell Drive Reston, Virginia 20191

To the Committee on Concrete Canoe Competitions,

The Michigan Technological University Concrete Canoe team wishes to express they have read and fully understand the 2023 request for proposals (RFP). Our team must design a prototype with a mix design, reinforcement scheme, hull design, and structural analysis completed for the proposed prototype. The team will also prepare a presentation and display for the prototype. The project proposal and MTDS addendum must be uploaded to the team's folder no later than 5pm EST, February 17th.

After taking an in-depth look at the RFP, the team would like to acknowledge the many changes to this year's competition. The Enhanced Focus Area (EFA) requirement has been removed from this year's RFP; however, the team acknowledges they are still free to focus on any topic beneficial to the progress of the team. With respect to the mix design, the amount of hydraulic cement is limited to 30% by mass and the volume of total aggregates is limited to 30% by volume. In addition to these requirements, the team must complete a sieve analysis of each individual aggregate and composite aggregate. This is our understanding of the rules for this year's competition.

We can't wait to bring our final prototype to competition this year. With knowledge transfer at the core of our values, we look forward to a successful year.

Sincerely, Michigan Technological University Concrete Canoe Team

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Lydia Lamey Team Captain llamey@mtu.edu 763-232-7085

Samuel Pendell Team Captain sjpendel@mtu.edu 989-475-1488

For al

Dr. Andrew Swartz ASCE Student Chapter Faculty Advisor raswartz@mtu.edu 906-487-2439



Pre-Qualification Form (Page 1 of X)

ARD SHARK

Michigan Technological University

(school name)

We acknowledge that we have read the 2023 ASCE Society-wide Concrete Canoe Competition Request for Proposal and understand the following (initialed by team project manager and ASCE Faculty Advisor):

The requirements of all teams to qualify as a participant in the ASCE Student Symposium and Society-wide Competitions as outlined in Section 3.0 and Exhibit 3.	JF	RAS
The eligibility requirements of registered participants (Section 3.0 and Exhibit 3)	18	RAS
The deadline for the submission of Letter of Intent, Preliminary Project Delivery Schedule and Pre-Qualification Form (uploaded to ASCE server) is November 4, 2022; 5:00 p.m. Eastern	J\$	RAS
The last day to submit ASCE Student Chapter Annual Reports to be eligible for qualifying (so that they may be graded) is February 1, 2023	JJ_	RAS
The last day to submit Request for Information (RFI) to the C4 is January 27, 2023	£8	RAS
Teams are responsible for all information provided in this <i>Request for Proposal</i> , any subsequent RFP addendums, and general questions and answers posted to the ASCE Concrete Canoe Facebook Page, from the date of the release of the information.	<i>}1</i>	RAB
The submission date of <i>Project Proposal</i> , and <i>MTDS Addendum</i> for the Student Symposium Competition (uploading of electronic copies to ASCE server) is Friday, February 17, 2023.	<i>Ŧ¥</i>	RAS
The submission date of <i>Project Proposal, and MTDS Addendum</i> for Society-wide Final Competition (bard copies postmarked to ASCE and uploading of uploading of electronic	11	RAS

Lydia Lamey 10/28/22 R. Andrew Swartz 10/28/22 (date) ASCE Student Chapter Faculty Advisor (date)

Lydia tomey

copies to ASCE server) is May 10, 2023; 5:00 p.m. Eastern.

(signature)



Pre-Qualification Form (Page 2 of X)

Michigan Technological University (school name)

As of the date of issuance of this Request for Proposal, what is the status of your school / university's 2022-23 classroom instruction (in-person, remote, hybrid)? What is anticipated after Thanksgiving and winter holiday break? If in-person or hybrid, do you have access to laboratory space or other facilities outside of classes?

Michigan Technological University is completely online for classroom instruction with no restrictions. It is anticipated that this will still be the case after Thanksgiving and winter holiday break. We have full access to a lab space.

In 250 words or less, provide a high-level overview of the team's Health & Safety (H&S) Program. If there is currently not one in place, what does the team envision their H&S program will entail? Include a discussion on the impact of COVID-19 on the team's ability to perform work and what plans would be implemented assuming work could be performed.

Our health & safety program is made up of two parts. Communication and prevention. We make sure to communicate with one another if we are not feeling well. This also ties into prevention. By continuing with open communication, we inherently prevent the spread of COVID-19. To continue preventing, we wear masks at all times when working in the concrete lab. Not only does this help stop the spread, but it's also an important measure we will take to protect our lungs from dust. In the lab, all members are required to wear proper PPE. We discuss new safety tips at each weekly meeting.

COVID-19 is not significantly impacting the team's ability to work at the moment. The most notable impact it has is the sudden absence of team members when they must quarantine.

In 150 words or less, provide a high-level overview of the team's current QA/QC Program. If there is currently not one in place, what does the team envision their QA/QC program will entail?

Quality control: The team uses depth gauges to ensure even layering of the canoe, checks humidity levels during the curing process, and checks for well mixed concrete during the casting and curing processes. After curing, the canoe is sanded and sealed.

Quality Assurance: All mixes and pre-batched and weighed to ensure they are meeting standards. Practices are held to make sure all members have casting experience prior to placement day.

Has the team reviewed the Department and/or University safety policies regarding material research, material lab testing, construction, or other applicable areas for the project?

All members of the team have completed a guided lab tour and lab safety training. All testing procedures have been reviewed.





The anticipated canoe name and overall theme is – (please provide a brief description of the anticipated theme. The intent is to allow ASCE to follow up to determine if there may be copyright or trademark issues to contend with, as well as to provide insight.)

Our overall theme is Vegas/Casino night. Our boat name has yet to be decided, but some options the team has discussed are Blitz or Card Shark. We intend to portray this with card suit inlays into the boat.

Has this theme been discussed with the team's Faculty Advisor about potential Trademark or Copyright issues?

The theme has been discussed and there should be no Trademark or Copyright issues.

The core project team is made up of 9 people.





Thank you to our advisors Dr. Tess Ahlborn

Dr. R. Andrew Swartz

Thank you to any additional members not mentioned

Adam Katers Brock Maloney Chris Eder Emily Mackintosh Jack Simons Kalib Perry Liam Silverman Lyza Brandner Pan Prathonkham Ryan Schumacher Tyler Parker Wes Reif

